How to Manage Pressure Loss in Injection Molding

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Ever encounter a part that has a process window thinner than a human hair?

Managing the pressure loss in the molding process is complicated and influenced by many factors that are outside the control of the molder. We must evaluate each of the following areas to ensure that the molder has a wide process window.

Part Design

Ultimately, the success of molding starts at the OEM. No matter the environment or application, a design engineer must understand how the geometry influences the success of each step along the way.

The thickness of the part plays an important role in how difficult the molding process will be. Typically, injection molded parts will be between 0.040 and 0.250 inches thick. Within this large range, we can divide them into three separate categories: thin, intermediate, and thick.

Another factor that can drastically influence the molding success is the how large the part is. To simplify this, we will use the overall length (OAL) of a part as an additional consideration. The OAL of injection molded parts can also vary widely, just like thickness. In the medical industry, some parts could be as short as 0.250 inches. In the automotive or appliance industry, the OAL could be 60 inches.

Each part has its own challenges, but for the focus of this article, we will evaluate a thinner walled part with a large OAL.

The example below is an A Pillar (**Figure 1**) for an automobile with a thickness of 0.080 inches and OAL of 55 inches.

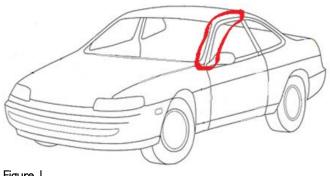
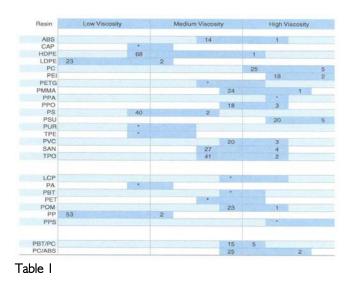


Figure I

Material Selection

The first step of selecting a material is to evaluate the viscosity characteristics. Remember, viscosity is measuring the internal resistance to flow. Certain materials, like polycarbonates, will always be a high viscosity resin and will require higher injection pressure from the molding machine to create flow.

Next, the focus shifts to the Melt Flow Index (MFI) or Melt Flow Rate (MFR). The MFI or MFR will give a reference to the flowability of a material within a given type of resin. If we review the data in **Table I**, we can see that there is a wide range of values for the flowability of each resin. When evaluating the MFI or MFR, it is imperative that a comparison is only done between the same types of resin (ABS to ABS, PC to PC , etc.).



If the material that is selected at the start of the project, is naturally a high viscosity resin, and has a low MFI or MFR, the risk of molding non-conformities increases drastically. Now for a brief message about the incoming lots of resin. There will be variation and likely lots of it. The viscosity can deviate $\pm 20\%$, depending on the quality of resin purchased. A typical virgin, wide spec resin will fall into this category. If there are additives, such as color or glass, the amount of variation can be greater than $\pm 20\%$. If regrind is added into the process, there can be viscosity shift of $\pm 40\%$.

In a typical automotive application, the A Pillar is molded out of PC/ABS or PC/ASA. Given that PC/ABS is a medium-high to high viscosity resin, the material selection increases the risk of consistently molding a quality product.

Mold Design

Now that we understand the size and material of the part to be molded, it's advisable to evaluate the mold design.

First, we must review the aspect ratio, which is a comparison of the flow length to wall thickness (expressed XXX: I). Flow length starts at the gate and ends at the furthest point from the gate within the cavity. A high aspect ratio increases the probability of molding non-conformities.

When there are multiple gates required within the same part, it's advised to balance the aspect ratio.

The size of the gate plays a crucial role in how well the material will flow. It also influences the ability to "pack out" the part. If the gates are too small, the injection pressure during fill will be very high, and the ability to pack out the part will be negatively impacted.

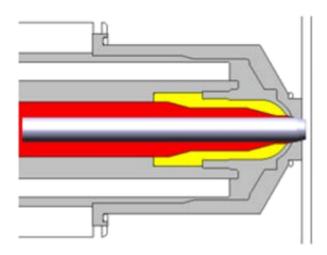


Figure 2

In our example of the automotive A Pillar, the material must flow 55 inches through a 0.080 inch thick wall, which yields an aspect ratio of 688:1. This ratio is extremely high if the part were to be single gated at one end. In this case, we would want multiple large gates strategically placed to reduce the aspect ratio. Also, since this part will likely be painted or chrome plated, knit lines are a concern. Given the cosmetic requirements, there is a good chance the mold would require sequential valve gates (SVG), shown in **Figure 2**.

Molding Machine

The performance requirements of the molding machine are essential to the success of any process. Here are three factors that need to be evaluated when selecting a machine:

- I. We must ensure that the injection unit has the correct volume to avoid un-melted pellets or degradation.
- 2. We must understand the volumetric flow rate this is critical. Thin wall parts require higher volumetric flow rate to ensure the cavity is filled prior to the flow front freezing. Depending on the age of the molding machine, volumetric flow rates can range from 5.0 in³/sec to 50 in³/sec.
- 3. We must consider the amount of plastic pressure a machine can produce in conjunction with volumetric flow rate. As the volumetric flow rate requirements increase, so does the plastic pressure required to achieve and maintain a desired volumetric flow rate. Again, taking into consideration the vintage of equipment, maximum injection pressure could be 20,000 PSIp to 45,000 PSIp.

Given what we know about the part geometry, material viscosity, and use of SVGs in the mold for the A Pillar, the flow rate would likely be around 8 in³/sec with peak plastic pressure during filling at near 25,000 PSIp.

Processing

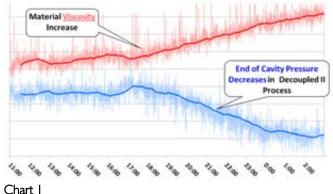
Over the years, RJG has learned that achieving a pressure at the end of cavity (EOC) of 3,000 PSIp

indicates the steps leading up to the process have allowed for a wide process window.

This is not to say that parts cannot be molded with less than 3,000 PSIp at the EOC, they can. However, the lower pressure that can be obtained at the EOC and the amount of risk associated with molding nonconformities increases exponentially.

In a DECOUPLED MOLDING[®] II process, if the viscosity of the material increases, the pressure at the EOC decreases, unless process changes are made. When pressure loss is greater than the validation, some molding non-conformities that can be expected are undersized dimensions, warp, sinks, and short shots.

In **Chart I**, the trend data from a 15-hour production run is displayed. The mold is equipped with cavity pressure sensors at the EOC, the machine is equipped with hydraulic pressure sensor to monitor shifts in viscosity, and the data is displayed on an eDART Summary Graph. Here the inverse correlation between viscosity and EOC peak pressure can be easily seen.



In the A Pillar application, we stated that the EOC has a peak of 3,000 PSIp at PPAP. If the viscosity increases by 20%, which is likely to occur over the life of the program, it could result in EOC peak of 1,800 PSIp. If no process adjustments are made, we could expect parts that are undersized, warped, or have sinks over thick sections.

If a DECOUPLED MOLDING III process strategy is selected, it can reduce the variation that is seen in the cavity when the material viscosity inevitably changes.

Conclusion

When trying to manage pressure loss, we must first consider the thickness and size of the part. Second, evaluate the MFI of the material against the geometry in which it must flow. Not only do we have to consider the MFI at the onset of the project, but the variation of material over time. Next, consider the mold design to ensure the aspect ratio is correct. Also, determine what the performance criteria is of the molding machine responsible for production. Finally, determine if the correct processing strategy was selected. If one of these critical areas is overlooked, it will be difficult to produce quality parts on a regular basis.

In short, if the part has a thin wall and long OAL and is running a high viscosity, low MFI resin, and a high aspect ratio, the likelihood of achieving 3,000 PSIp at the EOC is extremely low. A thorough evaluation of all the steps is required as well as a better process control method.



Jeremy Williams has over 16 years of experience in the plastics industry serving the medical, automotive, furniture, and appliance industries. He previously worked as a Principal Engineer, taking projects from design concept to saleable products. Jeremy

earned his Master Molder II certification in 2011, became an RJG Certified Trainer in 2012, and started at RJG in 2016. In addition to his extensive manufacturing background, he holds degrees in plastics and business.